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LOW-STRETCH AND DIMENSIONALLY STABLE FLOOR COVERING

Abstract:

A low-stretch and dimensionally stable floor covering (1) comprising polymer-containing pile material (2) which is retained to a polymer-containing primary backing (3), to the back of which an underlying secondary backing layer (5) is retained by means of an interleaving adhesive layer (4). The secondary backing layer (5) comprises a needled fibre structure of thermoplastic, polymer-containing, continuous or staple fibres being inter-fixated by heating. The adhesive layer (4) comprises an organic, polymer-containing binder which is activated by heat application. According to the invention, at least the secondary backing layer and/or the binder layer comprise a substantially re-usable material. After being formed, the carpet is wound onto so-called broadloom rollers and can, if desired, be cut partially into carpet tiles. Thus, carpet tiles and broadloom carpets can be manufactured in the same production process.

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(54) Title: LOW-STRETCH AND DIMENSIONALLY STABLE FLOOR COVERING			
(57) Abstract			
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Low-stretch and dimensionally stable floor covering

5 The present invention concerns a low-stretch and dimensionally stable floor covering comprising pile material which is retained to a primary backing layer to the back of which an underlying secondary backing layer is retained by means of an interleaving adhesive layer. The invention further concerns a method of manufacturing a floor covering of the kind stated in the
10 introduction and in which in an initial production step a web-formed semi-manufactured material is produced which comprises pile material being retained to a primary backing layer.

15 BACKGROUND OF THE INVENTION

Low-stretch and dimensionally stable floor coverings include wall-to-wall (also often called broadloom) carpets and carpet tiles exhibiting a low degree of shrinkage
20 and/or expansion lengthwise and/or widthwise, and consequently being highly capable of resisting varying moisture and heat impacts in use. Especially within the field of contract applications the dimensional stability of carpet tiles is to-day - due to their construction -
25 considerably higher than that of broadloom carpets. To compensate for the lower dimensional stability of broadloom carpets they are for contract applications to-day glued down to sub-floors by means of a permanent glue. Carpet tiles are only installed and glued down by means of
30 tackifier or are simply meant to be held in place by their high weight.

The known low-stretch and dimensionally stable floor coverings when used as wall-to-wall carpets comprise a
35 semi-manufactured material with pile material which is

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retained to a primary backing layer having a secondary backing layer which e.g. may consist of a coating of natural rubber, chalk-filled (calciumcarbonate-filled) SBR-latex foam or polyurethane foam or the like. These
5 backing layers are normally applied in a thickness of 2-8 mm. Because of their elastomeric properties foamed backing layers contribute significantly to the walking comfort. Additionally, the foamed backing layers also provide good temperature and sound insulation.

10 These known foamed backing layers, however, entail significant adverse environmental impacts, which are undesired in particular in the light of the present strict demands on environmentally friendly and re-usable
15 products. By re-usable products are meant products containing components which can be melted down and again enter into a production process, or components which by incineration give approximately nul residual ash percentage. The foamed backing layers often give off
20 residual gases for prolonged periods after production entailing risk of nuisance to the indoor climate in the room where the carpet has been laid out. At the same time it is a problem that the foamed backing layers after use for some length of time of the floor covering stick so
25 well to the underlying floor that the foamed backing layer often in very large areas is separated from the floor covering when worn-out floor covering is to be removed. The large areas with attaching remains of foamed backing layers must then be removed in a time-consuming working
30 operation before a new floor covering can be laid on the floor.

The most significant disadvantage of the known floor coverings with foamed backing layer, however, consists in
35 the limited possibilities of disposing of the used carpet coverings and the related unfortunate environmental

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impacts. In case of e.g. foamed chalk-filled SBR-latex backing coatings on worn out wall-to-wall carpets it is in practice at disposal only possible to achieve the level "incineration without energy recovery".

5 Chalk-filled foam backing layer contain a high concentration of inorganic materials which are left as ash after incineration.

The generally known carpet tiles are widely used in particular as so-called project carpeting, that is, carpet especially for contract areas and for industrial use. Understood herein by carpet tile is a regularly formed piece of carpet which (measured according to norms formulated for this purpose by inspection agencies such as

10 for instance TNO) has a shape and dimension stability sufficient to form a continuous floor covering under all conditions.

In such applications carpet tiles have great advantages compared with conventional broadloom carpets. The tiles are for instance easy to take up, whereby easy access can be obtained to the space under the floor for (re)positioning for instance computer and electricity cables. Carpet tiles can also be easily laid without unnecessary disruption of the normal activities in a room area. In addition, carpet tiles can be replaced locally in simple manner, which is advantageous when particular parts of a room area are used more intensively than others. They are also compact and therefore simple to transport,

20 particularly in high-rise office buildings where rolls of carpet can cause great transport problems.

The known carpet tiles are usually provided with a relatively heavy secondary backing layer and binder layer in order to ensure their shape and dimension stability.

35 The secondary backing layer is generally made of a strong

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coating of glass-reinforced bitumen or glass-reinforced PVC coating. The specific weight of a conventional carpet tile therefore amounts to roughly 5 kilograms per square metre.

5

A representative example of such carpet tiles is described in EP 0 278 690A2. In order to provide a carpet tile with good dimensional stability, good lay flat characteristics, and which may be produced by an in-line production method, a carpet tile is suggested, which comprises a fibrous face wear surface secured to a primary backing sheet,

10 a first precoat layer on the primary backing surface and comprising a hotmelt bitumen or petroleum resin composition,

15 a second precoat layer secured to the first coating layer and which second coating layer comprises a bitumen hotmelt composition,

20 a third coat backing layer which comprises a bitumen hotmelt composition, and

25 a secondary backing sheet material to provide dimensional stability to the carpet and secured to the third coating backing layer. Dimensional stability is achieved by the secondary backing comprising a woven or non-woven glass fibre scrim and by the high total weight of the tile.

In order to further improve the dimensional stability EP 0 420 661A2 describes a carpet tile comprising a wear surface and a primary backing comprising a

30 solid, hotmelt composition and a secondary backing composed of adjacent layers of a porous, glass fibre sheet material e.g. tissue, non-woven glass fibre and a porous, fibrous sheet material with a fibrous sheet material as the exterior surface of the secondary backing layer, and

35 wherein the hotmelt composition has penetrated and saturated the glass fibre material but has only partially

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penetrated the fibrous sheet material sufficiently to bond the fibrous sheet material. Typically, the carpet tile comprises a fibrous carpet material wherein the primary backing is a bitumen or a bitumen modified hotmelt composition. The secondary backing comprises separate, adjacent layers of a porous, lightweight glass fibre tissue sheet material which in itself gives the carpet tile the improved dimensional stability. According to the invention polypropylene, non-woven sheet material is in itself not a satisfactory material as a secondary backing carrier sheet.

EP 0 590 189A1 was filed on December 30, 1992 and published on April 6, 1994 (Art.54(3)EPC) for DE, FR, GB, and NL. It confirms the disadvantages of prior art carpet tiles comprising bitumen/asphalt backing members or PVC-backings.

According to one embodiment of this invention a tile-shaped carpet is provided which comprises a backing member and an upper layer formed on the backing member, both of which are made of a propylene resin. Preferably the upper layer includes a base fabric sublayer and a pile sublayer, both of which are made of propylene resin.

While reference is made to polypropylene fibres as part of the upper layer, the backing member is only described as being made of either propylene, monopolymer or copolymers of propylene and ethylene butene-1 and the like, which may comprise a regenerated product of the propylene resin. It is preferred to use an amorphous alpha-olefin copolymer and in fact the only embodiment specifically described is extrusion-moulded back-up members. The document comprises no reference to needled and textiled back-up members.

The known carpet tiles have a large number of drawbacks, however. The disposal and processing of the tiles at the end of their useful life thus causes great problems due to

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the nature and quantity of the materials used. When they are burned a significant portion, up to about 60% by weight, of the bitumen-containing tiles is left over in the form of ash.

5

Incineration of products such as tiles with PVC backing layers demands high energy supply during incineration, because PVC contains chlorine which uses energy during incineration instead of generating energy. Chlorine is also a toxic and etching gas which easily reacts with other inorganic and organic substances, wherefore incineration of floor coverings with PVC backing layer calls for special environmental measures during the incineration process.

15

It is moreover expected that the problems associated with the processing of waste tiles will become more pressing in the future since, with regard to the large numbers of carpet tiles laid and replaced annually (in Europe more than 40 million square metres with a weight of about 200,000 tons), legal requirements relating to the environmentally friendly processing thereof can be anticipated in the short term.

25

In addition, due to their comparatively heavy weight the known carpet tiles can only be simultaneously transported and laid in relatively small quantities. Moreover there is a considerable danger of back disorders for the carpet installers.

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As previously mentioned the construction of carpet tiles and broadloom carpets is totally different. Therefore, carpet tiles and broadloom carpet have conventionally been produced by different processes and on different types of manufacturing equipment. This has been due to the mentioned different materials which the carpet industry

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has had to use until now for meeting the application requirements for these two different products. For manufacturing carpet tiles the relatively stiff, heavy weight backing of bitumen or PVC with glass have been used, or for broadloom carpets the backing has conventionally been relatively flexible, been consisting of calcium carbonate filled foam or equivalent materials. So far it was therefore not possible to integrate the manufacture of these two types of carpets in one and the same process.

From EP 0547533 A1 a stretchable floor covering is known which when being laid out are often stretched by many percent lengthwise and widthwise, whereafter the edges of the stretchable floor covering are secured to adjoining panels by means of nail lists or the like. The secondary backing layer is instead of the previously known foamed coatings constituted by a backing layer with a fibre structure being embedded in or encompassed by a textile bonding so as to impart acceptable strength properties to the secondary backing layer for use as a stretchable floor covering. By the textile bonding is meant that the fibre structure may e.g. be needlepunched to an underlying strength imparting web, or that the fibre structure is provided with stitches or loops in the longitudinal and cross-sectional directions, e.g. according to the known Maliwatt or Kettenwirk principles. The specification, however, provides no directions for a backing layer with a fibre structure being sufficiently dimensionally stable in the longitudinal and cross-sectional directions for enabling production of a low-stretch and dimensionally stable floor covering possessing the same strength and dimensional stability properties and walking comfort as the known floor coverings with foamed backing layers and the same dimensional stability as the known carpet tiles.

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SUMMARY OF THE INVENTION

Consequently, it is the object of the present invention to provide a low-stretch and dimensionally stable floor covering possessing the same strength and dimensional stability properties and walking comfort as the known floor coverings, such as broadloom carpets having the undesired foamed backing layers and carpet tiles having glass scrim reinforced PVC- or bitumen-containing backing layers, and at the same time making it possible to avoid the undesired environmental impacts when disposing of the used floor coverings. The new floor covering should be applicable both as wall-to-wall carpets and as carpet tiles to be used optionally within the same fields, such as the contract areas, without the previously mentioned drawbacks for neither the wall-to-wall carpets nor the carpet tiles.

The low-stretch and dimensionally stable floor covering according to the present invention is characterized in that the backing layer comprises a needled fibre structure of thermoplastic, polymer-containing continuous fibres or staple fibres being inter-fixated by heating to a temperature which at least corresponds to the lowest softening temperature for the fibre materials in the fibre structure, and that the adhesive layer comprises an organic, polymer-containing binder which is activated by heat application and has a reaction temperature which is lower than the melting temperature for the majority of the fibre material content in the fibre structure.

The method of producing the low-stretch and dimensionally stable floor covering according to the invention is characterized in that a web-formed secondary backing layer comprising a needled fibre structure of thermoplastic, polymer-containing continuous fibres or staple fibres is

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heated to a temperature which at least corresponds to the lowest softening temperature for the fibre materials in the fibre structure, and that the back of the web-formed semi-manufactured material is joined with the web-formed secondary backing layer during the interleaving of an adhesive layer (precoat and binder layer) comprising an organic polymer-containing binder having a reaction temperature which is lower than the melting temperature for the majority of the fibre material content in the fibre structure and which is activated by heat application.

Hereby is achieved that it is possible to produce a low-stretch and dimensionally stable floor covering having a secondary backing layer of a needled fibre structure and having the same strength and stability properties both length-wise, widthwise, and cross-sectionally as well as walking comfort as the known floor coverings with the traditional undesired backing layers whether we are talking about wall-to-wall carpets or carpet tiles. The invention completely eliminates the environmental impacts at disposal as compared to the said known floor coverings. This applies for both wall-to-wall carpets and carpet tiles as these two floor covering products according to the invention are now identical.

By the invention it is surprisingly possible on the same equipment to produce a floor covering which optionally can be used as wall-to-wall carpets or as carpet tiles.

In view of the substantial thickness and the constitution of the tiles described in EP 0 278 690A2, EP 0 420 661A2, and EP 0 590 189A1, it was highly surprising that a satisfactory floor covering which is suitable both as broadloom and as carpet tiles could be obtained by leaving out the numerous layers of bitumen, glass fibres etc.

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In addition to the environmental advantages and a reduced consumption of materials etc. this invention is of great commercial value to the broadloom manufacturers who were not previously in a position to manufacture carpet tiles. This invention can be applied using existing equipment and, for a relatively low investment offers the broadloom manufacturer the opportunity to enter the market for carpet tiles.

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The secondary backing layer is made in that a thermoplastic needled fibre web of either continuous fibres or staple fibres is heated to the softening temperature of the fibres, whereby they are adhered together to form a backing layer having a three-dimensional mechanically cross-bonded fibre structure where the fibres are inter-fixated. The fibres, which are three-dimensionally oriented will during force impact and slackening (walking effect) counteract the tension and somewhat return to their original fibre structure. This property is called re-raising capacity (resilience). In the fibre structure according to the invention the individual fibres are connected and fixated to each other to form the three-dimensional fibre structure, which is to be seen in contrast to a fibre structure where the fibres are only retained to each other mechanically and may consequently slip away from each other during force impact so that the stability is significantly reduced and the re-raising capacity will quickly be lost. By inter-fixating the three-dimensional fibre structure stability and comfort in the secondary backing is increased.

Heat application to the fibre structure may be performed by calendering the fibre structure either on one side or on both sides or may be performed by blowing hot air through the fibre structure, or a combination of the said

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two thermal treatment processes. The heat application may also be performed by IR-radiation; i.e. treatment with infra-red rays or similar methods.

5 The fibre structure may both comprise continuous or staple fibres having a length of 20-200 mm and fibre thicknesses from 1.5dtex to 50dtex. Most often the choice will be staple fibres in the interval 40-110 mm fibre length and 3.3-20dtex fibre thickness. The weight of the fibre
10 structure of the secondary backing layer will essentially lie between 70g/m^2 and 1000g/m^2 , in particular between 100g/m^2 and 600g/m^2 . The heaviest backing layers are used for carpet for applications calling for particularly high walking comfort.

15 The fibre structure may be composed of fibre types which are used either 100% pure or in mixtures - and with varying thicknesses and lengths. Thus the fibre structure may consist of a mixture of natural fibres, such as wool,
20 cotton, flax or jute, and synthetic fibres, such as polymers and copolymers based on polyamide, polyester, polyolefines (polypropylene and polyethylene) or polyacrylates. Applicable copolyesters may e.g. be based on terephthalic acid and various polyglycols and/or other
25 aromatic carboxylic acids and alcohols. Applicable copolyamides may comprise 2, 3 or 4 different polyamides, e.g. polyamide 6, polyamide 6,6 and polyamide 12. The presently preferred thermoplastic polymer is polypropylene.

30 In order to obtain sufficient stability and strength in the fibre structure it must normally contain a fibre content of at least 25% of the thermoplastic polymer. The higher the number of thermoplastic polymers, the
35 higher the dimensional stability.

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Thus fine results are obtainable as regards both walking comfort and re-raising capacity of the secondary backing layer when the fibre structure has a fibre content of 100% identical thermoplastics or a fibre content of mixtures of thermoplastics within the same group of polymers or different groups of polymers, but with different softening temperatures. A fibre content of a polymer with a lower softening temperature can thus be utilized to increase the thermal bond to the remaining fibre content.

10

The fibres with the lowest softening temperatures and melting points will act as binders during heat application, while the fibres with the higher softening temperatures remain intact. The softening temperature differences between the various fibre types must normally be at least 10 °C for the said property to be utilized.

15

According to the invention the fibre structure may comprise fibres which are produced from a combination of two different fibre material types, the core of the individual fibres being constituted by one fibre material type, and the surface being constituted by a modified or other fibre material type.

20

The adhesive layer, which according to the invention comprises an organic, polymer-containing binder, may be an emulsion binder of an aqueous solution of polymer particles, or may be 100% thermoplastic binders also known as hot melt/powder adhesives. The binder may be chemically reactive and comprise polymers and/or copolymers of e.g. polystyrene butadiene, polyacrylate, polystyrene acrylate, polyvinylacetate, copolyamides, copolyesters or nitrile butadiene, and may further comprise a thermoplastic filler. In the case of a thermoplastic binder comprising polymers and/or copolymers of polyolefines, polyesters or polyamides, this may during

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the production be dispersed in a suspension to a pasta, or may be used as it is. Presently preferred binders are SBR-latex and polyacrylic latex with a polyethylene filler.

5 In the case of emulsion binders they will by means of capillary transportation diffuse into the back of the primary backing layer of the semi-manufactured material, and further diffuse into the upper side of the fibre structure of the secondary backing layer, and during the
10 succeeding heat application the binder is activated so as to achieve the fine retention. In particular when the surfaces of the fibre structure of the secondary backing layer are untreated and piled good penetration will be achieved and consequently good retention of the binder.

15 The materials in the secondary backing and the adhesive layer are preferably moisture-proof polymers. This is advantageous as the carpet during use will not change dimensions when exposed to humidity and heat fluctuations.
20 The stability of the carpet covering is thus ensured, while the weight thereof remains relatively low. The low weight of the backing construction (binder and adhesive layer) and the fact that the carpet can be rolled up easily moreover result in new and advantageous
25 possibilities with regard to the manufacture thereof.

According to the invention the stiffness and the material of the backing and the binder layer are chosen such that the thus formed carpet has a sufficient stability for
30 application both as carpet tile and wall-to-wall carpet and a comparatively low weight and, after being formed, the carpet is wound onto so-called broadloom rollers and cut partially into carpet tiles.

35 A particularly strong adhesion between the semi-manufactured layer and the secondary backing layer is

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obtainable by establishing a stabilizing synergistic effect between the binder and the fibre structure of the secondary backing layer. Such synergistic effect may e.g. be provided by the fibre structure comprising fibres where the polymeres have mutually different softening temperatures, and where the binder reaction temperatures at least lie between the softening temperature and the melting temperature of the first-molten fibre polymer in the fibre structure. Hereby the binder, when penetrating into the surface of the fibre structure, will react and bond together with the said first molten fibres. Hereby both the fibre structure and the binder contribute to adhesion. Simultaneously a strength imparting stabilization of the carpet covering is achieved.

In addition to the said positive properties provided by the adhesives (precoat and binder) and the secondary backings of the invention in terms of the mechanical dimensional stability of the carpet, they are also of great importance to the dimensional stability of the carpet in terms of climatic changes.

One of the main problems in relation to climatic dimensional stability is that the semi-manufactured material e.g. comprising polyamide or wool "pile materials" even though constructed on dimensionally stable primary backings will shrink and extend due to changes in temperature and humidity.

Previously this problem regarding dimensional stability is solved by use of the glass fibre reinforcement layers or heavy backing layers of bitumen or PVC mentioned in the "Background of the Invention".

By the carpet construction according to the invention is on the contrary achieved a saturation of the stabilizing

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part of the carpet with moisture proof polymers. The saturation with these polymers is in all embodiments of the new carpet sufficient to prevent degradation of stability due to moisture penetration.

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Especially good dimensional stability is obtained when the secondary backing consists of no-moisture absorbent materials and the main part of the adhesive layer consists of no-moisture absorbent polymers after bonding thereof. The saturation is obtained by the adhesive layer which penetrates into the backside of the semi-manufactured material and the secondary backing as previously described. The saturation of the carpet construction can be sufficient to build up a waterproof membrane or can be just sufficient to allow a certain air permeability through the carpet.

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For contract applications the carpet will in practice primarily be based on thermoplastic and non-moisture absorbing materials in the adhesive and the secondary backing layer.

20

It appears from the above description that the same types of thermoplastic polymers are applicable as fibres and adhesives to a great extent. The person skilled in the art will be able to select the proper ingredients without undue experimentation in order to obtain the proper melting characteristics depending on whether e.g. a fibre, a hot melt adhesive or a thermoplastic filler for the adhesive is desired. Typically the exact formulation is chosen by the supplier in accordance with the specified properties.

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According to the invention special environmental advantages are obtainable at disposal of the floor covering. When the entire floor covering construction,

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i.e. pile, primary backing layer, binder and back are made from organic polymers, the floor covering used can be incinerated by a controlled incineration with energy recovery. As mentioned above, it may be a case of pure thermoplastic polymers and copolymers of e.g. polyesters, polyamides, polyacrylates etc., and/or natural materials, such as flax, cotton, jute and wool, and combinations thereof. In many countries, like in Denmark, use is made of incineration with energy recovery when disposing of waste, such as used carpet coverings.

According to the invention possibility is also offered in a particularly advantageous way of melting down the used floor covering or treating it chemically so that afterwards it can be used in the production of new fibre floor coverings or other products. In this connection the entire floor covering construction comprising pile, primary backing layer, binder and secondary backing layer is to be produced from mutually re-cyclable compatible materials. Use can e.g. be made of 100% polyolefines (polyethylene/polypropylene), a 100% polyester based floor covering construction or a construction based on polyamides. It will be especially advantageous if the binder is constituted by 100% thermoplastic materials.

BRIEF DESCRIPTION OF THE DRAWINGS

In the following the invention is explained in more detail, reference being made to the various embodiments and the drawings in which

Fig. 1 shows a schematical section of the floor covering according to the invention where the primary backing layer comprises a woven material,

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Fig. 2 in the same way as in Fig. 1 shows another embodiment where the primary backing layer comprises a non-woven fibre structure,

5 Fig. 3 shows the process steps according to the invention for producing the floor covering,

Fig. 4 shows a section through a part of a carpet tile according to the invention,

10

Fig. 5 shows schematically an example of a method of manufacture according to the invention, and

15 Figs. 6-12 show Differential Scanning Calorimetry (DSC) curves for a representative selection of applicable polymer materials in the floor coverings according to the invention as further described below.

20

DETAILED DESCRIPTION OF THE INVENTION

In case of the floor coverings 1 and 1' shown in figs. 1 and 2 a web-formed semi-manufactured material is produced in an initial production step, which material comprises polymer-containing pile material 2 and 2' being retained to a polymer-containing primary backing layer 3 and 3'. As mentioned in the introduction both the pile material and the primary backing layer may comprise both natural fibres and synthetic fibres, or mixtures thereof. In the embodiment shown in Fig. 1 the primary backing layer 3 is constituted by a woven primary backing layer, and the pile material is a looppile 2. In the embodiment shown in Fig. 2 the primary backing layer 3' is constituted by a fibre structure e.g. a known spunbonded fibre structure, and the pile material is a cutpile 2'.

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5 The web-formed semi-manufactured material 2, 3 or 2', 3' is joined with the underlying secondary backing layer 5, 5', respectively, by means of an interleaving adhesive layer 4, 4', respectively, and with simultaneous heat application to form the web-formed floor covering 1, 1', respectively, according to the invention. The web-formed floor covering is subsequently cut into wall-to-wall carpets or carpet tiles with the desired sizes.

10 The organic polymer-containing binder 4, 4', respectively, which is activated by a heat application, has a reaction temperature which is lower than the melting temperature for the majority of the fibre material content in the fibre structure. By the application of heat the binder is
15 heated to a temperature in the interval 60-250 °C, the heat application of course depending on the reaction temperature of the binder, which is adapted to the melting temperature for the majority of the fibre material type in the fibre structure, as will be explained in the
20 following.

As previously mentioned the emulsion binders may be in the form of polymeric particles in aqueous solution, the emulsion binders can be divided into the groups chemically
25 reactive binders and thermoplastic binders. The chemically reactive emulsion binders may be based on base polymers and copolymers of polystyrene butadiene, polyacrylate, polystyrene acrylate, polyvinylacetate and nitrile butadiene. As regards the thermoplastic emulsion binders
30 they are thermoplastics dispersed in suspension to a pasta. The thermoplastics may be based on polymers and copolymers of polyolefines, polyester, polyamides etc. This type of binder is especially used when it is desired to be able to re-cycle the floor covering and the
35 materials in the composite construction. E.g. polyolefine-containing binder is used when the carpet construction

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contains polypropylene and/or polyethylene fibres.

5 The adhesives may also be present in the form of 100% pure thermoplastics based on polymers and copolymers of polyolefines, polyesters and polyamides. The thermoplastics are applied onto the semi-manufactured material and the fibre structure of the secondary backing layer in dry state. Use may be made of several different application and lamination methods, e.g. powder application or melt application (hot melt).

15 By the powder application the thermoplastic binder is applied in powder form between the web-formed semi-manufactured material and the web-formed secondary backing layer, whereafter the layers are pressed together under heat impact, so that the thermoplastic is activated, melts and adheres the two layers to the finished web-formed floor covering material.

20 By melt application the thermoplastic binder is heated to a liquid mass which is positioned e.g. by extrusion between the web-formed semi-manufactured material and secondary backing layer which subsequently are pressed together e.g. between rollers. Under subsequent cooling the liquid binder hardens, and the two layers are retained fixedly together to the finished web-formed floor covering material.

30 The binders consisting of 100% thermoplastic materials are used particularly advantageously when the floor covering is composed of mutually compatible and consequently recyclable materials.

35 Furthermore, it is important to indicate that the adhesive layer can comprise several layers - laid on one by one. For example can a layer of polyacryllatex comprising a

- 20 -

polyethylene filler be laid as a precoat layer whereafter a hotmelt layer or a powder adhesive layer of polyethylene can be laid as a secondary adhesive layer. Another example could be applying a hotmelt layer as a precoat with a lower viscosity than the preceding binder layers (hotmelt or powder layers).

In the following the composition of the secondary backing layer 5, 5', respectively, is explained.

10

A typical construction of the backing layer is a fibre structure having a weight of about 300 g/m^2 , with 80% polypropylene fibres having a length of 60-100 mm in approx. 5-15dtex and 20% stretched out high density polyethylene fibres having a length of 60-100 mm in 7-20dtex. By blowing through the fibre structure with hot air of approx. 110-140 °C the non-stretched HDPE-fibres are softened, and contract additionally 30%. The polypropylene fibres are not influenced during the blowing through with hot air. The HDPE-fibres contract around and adhere to the PP-fibres which hereby are fixed and locked in the fibre structure. Hereafter the back of the fibre structure may be calendered. Hereby a fibre structure is created which possesses both vertical strengths and dimensional stability as well as horizontal stability.

In another typical embodiment of the secondary backing layer the fibre structure has a weight of 600 g/m^2 and comprises 100% polypropylene fibres. Here a broad molecular weight distribution in polypropylene is utilized - the shorter molecule chains are first softened and utilized for adhering together and fixation of the fibres.

The fine strength and dimensional stability properties of the secondary backing layer are thus achieved by the said inter-fixation of the fibres in the structure. The

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calendering of the back contributes to a homogeneous surface without loose-hanging fibre material. Hereby the finished floor covering material can be fixedly adhered to underlying floor or foundation by existing adhesion methods, such as double-adhering tape, tackifiers or glue. It is a further advantage of the homogeneous surface that the back visually has been imparted with an even textile-like surface which may contribute in making the finished floor covering more exclusive in connection with sale and marketing.

Embossing and printing on secondary backing can also be means to improve the visual appearance of the floor covering.

The installation of broadloom carpets having a construction according to the invention gives a number of advantages. The fact that the broadloom carpet of the invention has a dimensional stability similar to that of carpet tiles and that it has a homogenous surface makes it possible to install it by using tackifier as opposed to the technique applied to-day where broadloom carpets are glued down to the sub-floor by means of a permanent glue. The reason why permanent glue is used to-day is that broadloom carpets which contain chalk etc., shrink and extend due to changes in temperatures and humidity. If a tackifier is used on such a carpet, unstability and subsequently wrinkles may occur. If a tackifier is used in connection with installation of broadloom carpets according to the invention, major cost savings are achieved due to reduced binder quantity and the fact that the binder is easily removed after use. Thus problems in connection with removal of permanent glue, levelling and repair of sub-floors are avoided.

It should be mentioned that for such uses of floor

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covering which call for low electrical surface and transition resistance, e.g. lower than 10^9 ohm the fibre structure may be admixed with easily conducting fibres, or be impregnated with an easily conducting liquid. By use of
5 as much as 5% of either steel fibres or cobber and nickel coated fibres, or by the said impregnation of the fibre structure by approx 0.8% of an easily conducting liquid, the backing may be imparted with electrical surface-transition resistance down to 10^6 ohm measured according
10 to DIN 54345.

A carpet tile 11 (figure 4) comprises a secondary backing layer 12, a binder layer 13 and a top layer 14. The last-mentioned consists of a primary backing layer 15 and
15 threads 16 stitched therein. Secondary backing layer 12 and binder layer 13 are relatively flexible and light and each comprise re-usable material, for example a re-usable polymer.

20 The re-usable polymer of the secondary backing layer 12 and/or binder layer 13 can be moisture-proof. The shape and dimension stability of tile 11 is hereby increased considerably, as the material of the secondary backing layer 12 and/or binder layer 13 can then absorb
25 practically no moisture. Backing 12 can be manufactured for this purpose of for instance non-woven polypropylene, while as binder 13 can be used a mixture of latex and polyethylene. The exact mixing ratio of the binder components can be varied in order to obtain specific
30 properties in specific carpet constructions. An exemplary mixture might e.g. contain 40% SBR latex and 60% polyethylene. To increase the stability of tile 11 a material is preferably used for the primary backing layer 15 which corresponds closely with secondary backing layer
35 12 in respect of its most important properties. A suitable choice in this case is a primary backing 15 of

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5 spun bonded polyester. The above materials not only result in a stable carpet tile 11 which is moreover to a very great extent reusable, whereby a significant reduction of the amount of waste for dumping or burning is already achieved, but they also result in a considerable reduction in the tile weight per se, whereby the amount of waste is reduced still further. Other combinations of materials and layer thicknesses are of course also conceivable with which a stable, easily processed and light tile 11 is
10 obtained.

The specific weight of secondary backing layer 12 can for instance be in the order of 300 grams per square metre through use of the above described materials, while binder
15 layer 13 can have a specific weight of for instance about 900 grams per square metre. Herewith the secondary backing 12 and binder layer 13 in this embodiment together represent between 35 and 70% of the total tile weight, since a typical top layer 14, which may have a thickness
20 of several millimetres, will have a specific weight in the order of 500-2,000 grams per square metre (in the embodiment roughly 1,100 grams per square metre for the threads 16 and about 100 grams per square metre for the primary backing 15). The specific weight of the carpet
25 tile 11 thus amounts in total to roughly 2.4 kilograms per square metre, therefore approximately half a conventional carpet tile. By selecting re-usable material for secondary backing 12 and/or binder layer 13, less than 200 grams per square metre of the original material remains for dumping
30 after use and incineration.

Because the material of carpet tile 11 is relatively flexible and light it is simple to roll up. This makes it possible to wind the carpet onto broadloom rollers and
35 supply it either as broadloom carpets or as carpet tiles, whereby for instance a relatively little used part of a

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floor of a room area can be fitted with broadloom carpet, while a more intensively used part of the area, for instance a passageway, can be laid with identical carpet tiles which after a period of time can be easily replaced. Considerable savings are thus achieved in carpeting costs while the quantity of waste material is also greatly limited in this way.

A method of manufacture wherein carpet is produced in these two forms is depicted schematically in figure 5. Herein the separately formed secondary backing 12 and top layer 14 wound onto rollers 17 and 18 respectively are pressed onto one another between two pressure rollers 19 after a layer of binder 13 has first been applied to the top layer 14 from a reservoir 20 with an outlet opening 21. The carpet 22 obtained between the pressure rollers 19, optionally after heating or drying, is finally wound onto broadloom rollers 23 and at a later stage optionally partly cut into carpet tiles 11. A producer can thus supply in simple and inexpensive manner two well matched products, i.e. broadloom carpet and identical carpet tiles cut therefrom.

In the following examples are given of specific constructions of the fibre structure of the secondary backing layer:

- 1.1
Weight: 300 g/m²
Material: 100% polypropylene (DSC curve fig. 6)
Fibre mixture: 5/11/15dtex, 60/70/80/90 mm
Heat treatment: Calendering on the back within the temperature interval 150-190 °C.
- 1.2
Weight: 300 g/m²

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- Material: 70% polypropylene (DSC curve fig. 6)
and 30% polyethylene (DSC curve fig. 7)
- Fibre mixture: Polypropylene 5/11/15dtex, 60-100 mm
Polyethylene 7-20dtex, 60-100 mm.
- 5 Heat treatment: A) Blowing through with hot air in the
temperature interval 130-150 °C
B) Calendering on the back at 140-180
°C.
- 10 1.3
- Weight: 600 g/m²
- Material: 70% polyester (PET, DSC curve fig. 8)
and 30% copolyester (DSC curve fig. 9)
- Fibre mixture: Polyester 7/15dtex, 60-80 mm
- 15 Copolyester 6,7dtex, 60-80 mm
- Heat treatment: A) Blowing through with hot air in the
temperature interval 150-230 °C.
B) Calendering on the back at 200-260
°C.
- 20 1.4
- Weight: 600 g/m²
- Material: 70% polyamide 6 and 20% copolyamide
(DSC curve fig. 10)
- 25 Fibre mixture: Polyamide 6 5/11/15dtex, 60/80 mm
Copolyamide 4,2/11dtex, 50/80 mm
- Heat treatment: IR-radiation in the temperature
interval 120-220 °C.
- 30 In the following examples are given of expedient
embodiments of the floor covering according to the
invention:
- 2.1 (5/32 gauge looppile)
- 35 Pile material: 100% polypropylene, filament yarn, 650
g/m²

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- Primary backing
 layer: 100% polypropylene, woven 120 g/m^2
 Adhesive layer: 100% polyethylene melt adhesive
 (supplied by Hüls AG, Germany, or Dow
 Chemical, USA) 400 g/m^2
- 5 Secondary backing
 layer: As in example 1.1, the weight may,
 however, be larger, e.g. 450 g/m^2 .
 Total weight: 1620 g/m^2 , see fig. 1.
 10 Disposal level: Material recycling by melting.
- 2.2 (1/8 gauge cutpile)
 Pile material: 100% polyester spun yarn 800 g/m^2
 Primary backing
 15 layer: 100% polyester spunbonded 120 g/m^2
 Adhesive layer: 100% copolyester melt adhesive
 (supplied by Ems Chemie, Domat-Ems,
 Switzerland, under the trade name
 Griltex 11) 400 g/m^2
- 20 Secondary backing
 layer: 100% polyester 500 g/m^2
 Total weight: 1820 g/m^2 , see fig. 2.
 Disposal level: Partial material recycling by melting
 and chemical treatment.
- 25 2.3 (1/10 gauge cutpile)
 Pile material: 100% polyamide-filament yarn 1100 g/m^2
 Primary backing
 layer: 100% polyamide woven 140 g/m^2
 30 Adhesive layer: Paste adhesive based on copolyamide
 (supplied by Ems Chemie, Domat-Ems,
 Switzerland, under the trade name
 Griltex 8) 250 g/m^2
- Secondary backing
 35 layer: 100% polyamide 600 g/m^2 or as in
 example 1.4

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Total weight: 2090 g/m², see fig. 1.
Disposal level: Partial material recovery by melting down and chemical treatment.

5 2.4 (1/4 gauge looppile)

Pile material: 100% polyamide-filament yarn 1000 g/m²

Primary backing

layer: 100% polypropylene woven 120 g/m²

10 Adhesive layer: Modified pre-coat 800 g/m² and modified binder 480 g/m² based on carboxylated styrene acrylate copolymer with polyethylene filler (supplied by Dow Benelux, Tessenderlo, Belgium)

Secondary backing

15 layer: As in example 1.1

Total weight: 2700 g/m², see fig. 1.

Disposal level: Energy recovery by incineration.

2.5 (1/10 gauge cutpile)

20 Pile material: 100% wool, 1100 g/m²

Primary backing

layer: 100% polypropylene woven 120 g/m²

25 Adhesive layer: Modified pre-coat 750 g/m² and modified binder 450 g/m² based on carboxylated styrene butadiene copolymer with polyethylene filler (supplied by Dow Benelux, Tessenderlo, Belgium)

Secondary backing

layer: As in example 1.1

30 Total weight: 2720 g/m², see fig. 1.

Disposal level: Energy recovery by incineration.

2.6 (1/8 gauge cutpile)

35 Pile material: 100% polyamide, filament yarn 1100 g/m²

Primary backing

layer: 100% polyester, spun bonded 120 g/m²

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- Adhesive layer 1: Modified precoat based on carboxylated
styrene acrylate copolymer
(supplied by Dow Benelux) 450 g/m²
- Adhesive layer 2: 100% polypropylene melt adhesive
(supplied by Hüls/Dow) 200 g/m²
- Secondary backing: As in 1.1, the weight may, however,
be larger, e.g. 600 g/m², 450 g/m²
- Total weight: 2320 g/m².
- 2.7 (5/32 gauge looppile)
- Pile material: 100% polypropylene, filament yarn
600 g/m²
- Primary backing: 100% polypropylene, woven 100 g/m²
- Adhesive layer 1: Modified precoat based on carbox-
ylated styrene acrylate copolymer,
polyethylene as filler
(supplied by Dow Benelux) 400 g/m²
- Adhesive layer 2: 100% polyethylene melt adhesive
(supplied by Hüls/Dow) 200 g/m²
- Secondary backing: As in 1.1, the weight may, however,
be larger, e.g. 450 g/m², 300 g/m²
- Total weight: 1600 g/m².
- 2.8 (1/10 gauge cutpile)
- Pile material: 100% polyamide, spun-yarn 800 g/m²
- Primary backing: 100% polyester, spunbonded 120 g/m²
- Adhesive layer 1: modified precoat based on carbox-
ylated styrene acrylate copolymer,
polyethylene as filler and 300 parts
aluminiumhydroxide
(supplied by Dow Benelux) 600 g/m²
- Adhesive layer 2: 100% polyethylene melt adhesive
(supplier Hüls/Dow) 200 g/m²
- Secondary backing: As in 1.1, the weight may, however,
be lower, e.g. 450 g/m², 600 g/m².

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Total weight: 2320 g/m².

2.9 (1/8 gauge cross over cut)

Pile material: 100% polyamide, filament yarn, 1000 g/m²

5 Primary backing: 100% polyester, spunbonded 120 g/m²

Adhesive layer 1: Modified precoat based on carbox-
ylated styrene acrylate copolymer,
polyethylene as filler and 200 parts
aluminiumhydroxide

10 (supplied by Dow Benelux) 600 g/m²

Adhesive layer 2: 100% polyethylene powder adhesive
(supplied by Hüls/Dow), 200 g/m²

Secondary backing: As in 1.1 the weight may, however,
be lower, e.g. 300 g/m², 450 g/m².

15 Total weight: 2370 g/m².

As previously mentioned the fibre structure can
advantageously be made from a combination of two different
fibre material types, where the core of the individual
20 fibres is constituted by one fibre material type, and a
surface is constituted by another fibre material type (bi-
component fibres). E.g. fibres with polypropylene core and
with a polyethylene surface may be used. DSC-curve for a
typical fibre of this type is shown on fig. 6. Use may
25 also be made of polyester fibres with polyester core
having a melting point of about 256 °C and with polyester
having a melting point of about 225 °C, DSC-curve for a
typical fibre of this type is shown on fig. 7, or with
another polyester composition having a melting point e.g.
30 of 140 °C.

Testing of samples of floor covering embodiments
according to the examples 2.1-2.9 has been carried out and
compared with conventional bitumen tiles by the Danish
35 Technological Institute according to ISO 34551/1-1981(E)
with a view to determining residual ash percentage at

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total incineration at 600 °C. A representative example of the results are shown in Table A.

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TABLE A

5	Ash, percentage by mass of the Conventional bitumen carpet tile		
10	Test no.	Total sample, incl. pile and under part	Under part of the sample *)
	1	45.9	65.2
	2	44.3	65.8
	Mean values	45.1	65.6
15	Mass of test specimen approx. 4.5 g approx. 3.0 g		
20			
25	Ash, percentage by mass of the New Development		
	Test No.	Total sample, incl. pile and under part	Under part of the sample *)
	1	0.9	1.0
30	2	0.9	1.0
	Mean values	0.9	1.0
	Mass of test specimen approx. 1.8 g approx. 0.4		
35	*) The pile was separated from the under part of the adhesive layer.		

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Many changes can be made without departing from the idea of the invention. Thus, many different material combination may be used in the composite layers of the floor covering as long as the secondary backing layer comprises a needled fibre structure of thermoplastic polymer-containing fibres being inter-fixated by heating, and as long as the adhesive layer comprises a polymer-containing binder which is activated by heat application.

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C l a i m s :

- 5 1. A low-stretch and dimensionally stable floor covering
(1) which comprises
- a primary backing layer (3)
- 10 a pile material (2) retained to said primary backing layer
(3)
- 15 an underlying secondary backing layer (5) comprising a
needled fibre structure of thermoplastic, polymer-
containing continuous or staple fibres which are inter-
fixated by heating to a temperature at least corresponding
to the lowest softening temperature for the fibre
materials in the fibre structure,
- 20 said secondary backing layer (5) being retained to the
back of said primary backing layer (3) by means of an
interleafing adhesive layer (4) comprising an organic,
polymer-containing binder which is activated by heat
application and has a reaction temperature which is lower
25 than the melting temperature for the majority of the fibre
material content in the fibre structure.
- 30 2. A floor covering according to claim 1, wherein the
content of the thermoplastic, polymer-containing fibre
materials constitutes at least 25% of the fibre structure
in the secondary backing layer (5).
- 35 3. A floor covering according to claim 1, wherein the
thermoplastic, polymer-containing fibre materials are
selected from the group consisting of polypropylene,
polyester, polyamide, polyethylene, copolymers hereof, and
combinations hereof.

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4. A floor covering according to claim 1, wherein the thermoplastic, polymer-containing fibre materials comprise at least two fibre material types having a softening temperature difference of at least 10 °C between the fibre material type with the lowest softening temperature and the fibre material type with the second lowest softening temperature.

5. A floor covering according to claim 1, wherein the fibre structure comprises fibres which are produced by a combination of two different fibre material types (bi-component fibre), the cores of the individual fibres being constituted by one fibre material type, and surface being constituted by another fibre material type.

6. A floor covering according to claim 1, wherein the binder of the adhesive layer (4) is an emulsion binder which is constituted by an aqueous solution of polymeric particles.

7. A floor covering according to claim 6, wherein the binder is chemically reactive and comprises polymers and/or copolymers of either polystyrene butadiene, polyacrylate, polystyrene acrylate, polyvinylacetate or nitrile butadiene.

8. A floor covering according to claim 7, wherein the chemically reactive binder comprises a thermoplastic filler.

9. A floor covering according to claim 6, wherein the binder is thermoplastic and comprises thermoplastics which during the production are dispersed in a suspension to a paste.

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10. A floor covering according to claim 1, wherein the binder is thermoplastic and during the preparation is applied in powder form, or during the production is heated to a liquid mass (hot melt).

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11. A floor covering according to one or more of the claims 8-10, wherein the thermoplastics comprise polymers and/or copolymers of either polyolefines, polyester or polyamides.

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12. A floor covering according to claim 1, wherein the secondary backing layer (5) has a weight of 70-1000 g/m².

15

13. Carpet tile provided with a secondary backing layer, a layer of binder and a top layer comprising a primary backing layer, characterized in that at least the secondary backing layer and/or the binder layer comprise a substantially re-usable material.

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14. Carpet tile as claimed in claim 13, characterized in that the re-usable material is a polymer.

25

15. Carpet tile as claimed in claim 13 or 14, characterized in that the re-usable material is moisture-proof.

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16. Carpet tile as claimed in any of the previous claims, characterized in that the secondary backing layer comprises polypropylene and the binder layer polyethylene.

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17. Carpet tile as claimed in any of the previous claims, characterized in that the top layer consists of a primary backing layer and threads stiched therein and the primary backing layer and the secondary backing layer each formed by a non-woven sheet.

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18. Carpet tile as claimed in claim 17, characterized in that the primary backing layer comprises polyester.

5 19. Carpet tile as claimed in any of the previous claims, characterized in that the secondary backing layer and the binder layer together have a specific weight of a maximum of 1,800 g/m².

10 20. A method of producing a floor covering according to claim 1, comprising the steps of

initially producing a web-formed semi-manufactured material comprising a pile material (2) which is retained to a primary backing layer (3),

15 heating a web-formed secondary backing layer (5) comprising a needled fibre structure of thermoplastic, polymer-containing continuous or staple fibres to a temperature which at least corresponds to the lowest softening temperature for the fibre materials in the fibre structure, and

20

25 joining the back of the web-formed semi-manufactured material (2, 3) with the web-formed backing layer (5) by interleaving an adhesive layer (4) comprising an organic polymer-containing binder having a reaction temperature which is lower than the melting temperature for the majority of the fibre material content in the fibre structure and which is activated by heat application.

30 21. A method according to claim 20, wherein the web-formed secondary backing layer (5) is heated by a calendering where the temperature essentially lies within the interval from 110 °C to 260 °C.

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22. A method according to claim 20, wherein the web-formed secondary backing layer (5) is heated by blowing through hot air to a temperature which essentially lies within the interval from 110 °C to 260 °C.

5

23. A method according to claim 20, wherein the web-formed secondary backing layer (5) is heated by radiation with infra-red rays to a temperature which essentially lies within the interval from 110 °C to 260 °C.

10

24.A method according to claim 20, wherein the interleaving of the binder comprises a pre-application of the binder on the back of the web-formed semi-manufactured layer (2, 3) or on the upper side of the secondary backing layer (5), prior to joining thereof.

15

25. A method according to claim 20 further comprising cutting the finished produced web-formed floor covering (1) at least crosswise of the direction of advance to form floor covering pieces in the desired size, e.g. for use as carpet tiles.

20

26. A method for manufacturing carpet by forming a top layer comprising a primary backing layer, forming a secondary backing layer and bringing together and, by interposing a bonder, mutually joining the top layer and the secondary backing layer, characterized in that the stiffness and the material of the secondary backing layer and the binder layer are chosen such that the thus formed carpet has a sufficient stability for application as carpet tile and a comparatively low weight and, after being formed, the carpet is wound onto so-called broadloom rollers and cut partially into carpet tiles.

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27. Installation of carpet according to any of the previous claims to an underlying floor by use of

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tackifier.

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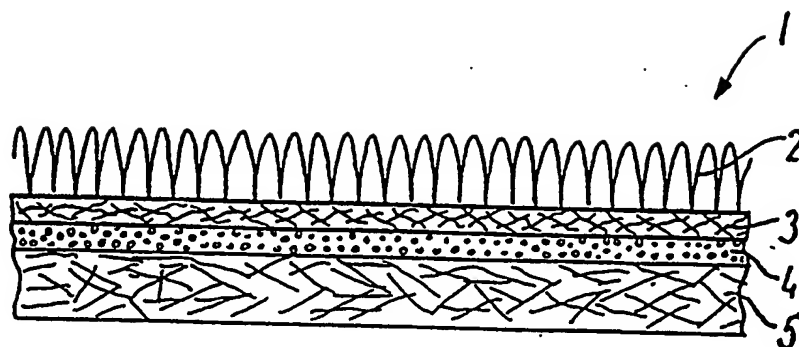


FIG. 1

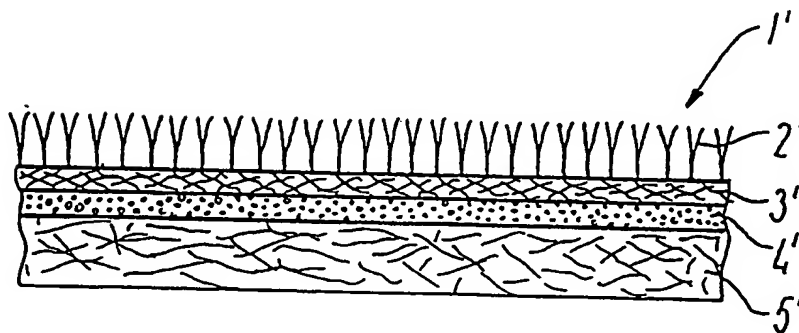


FIG. 2

2/11

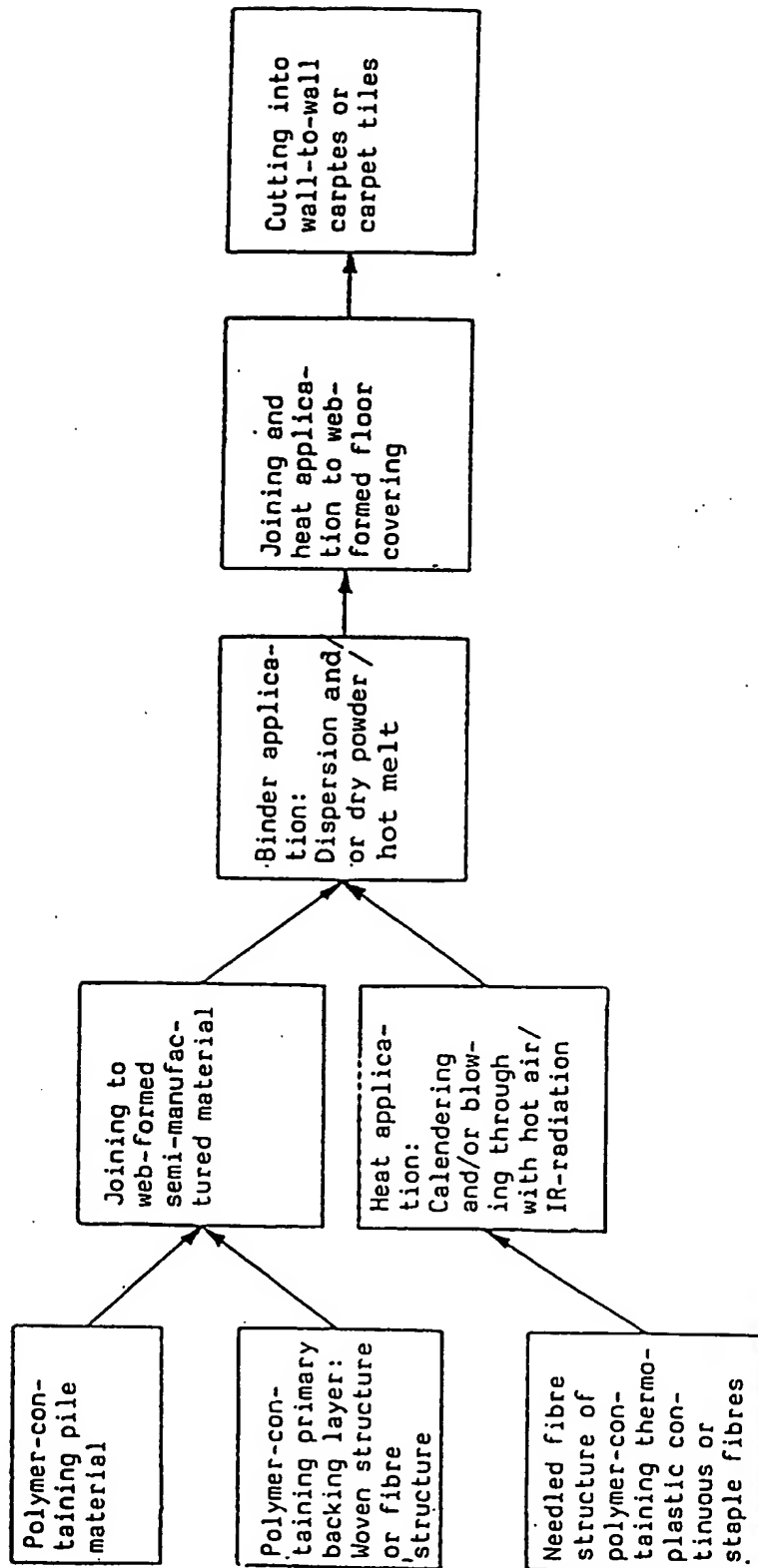


FIG. 3

3/11

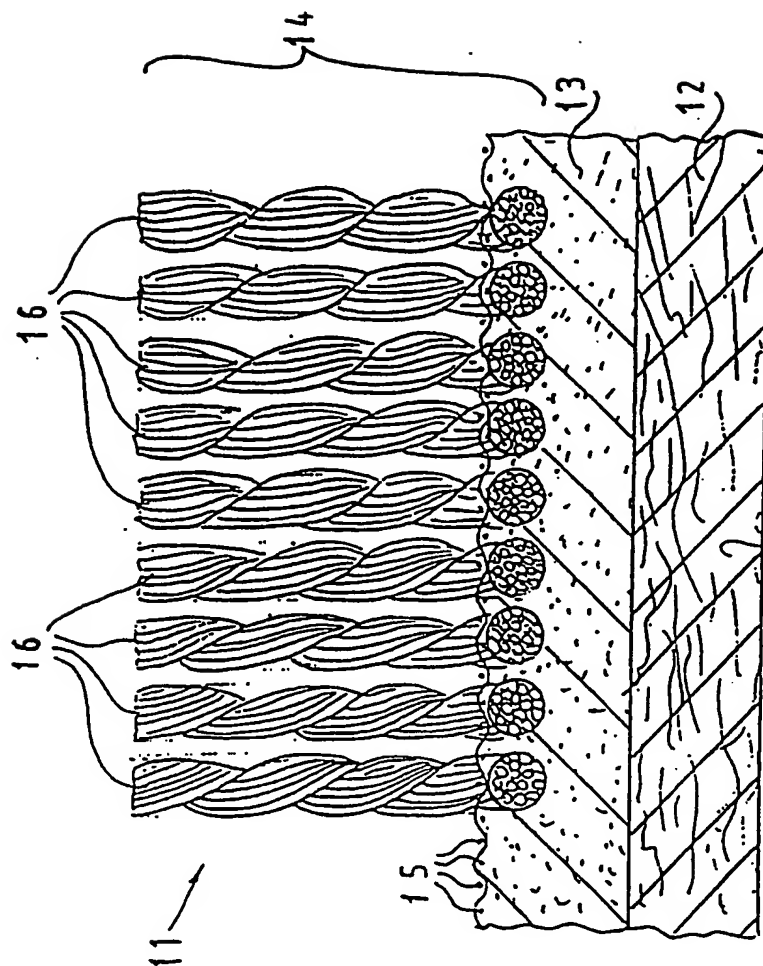


FIG. 4

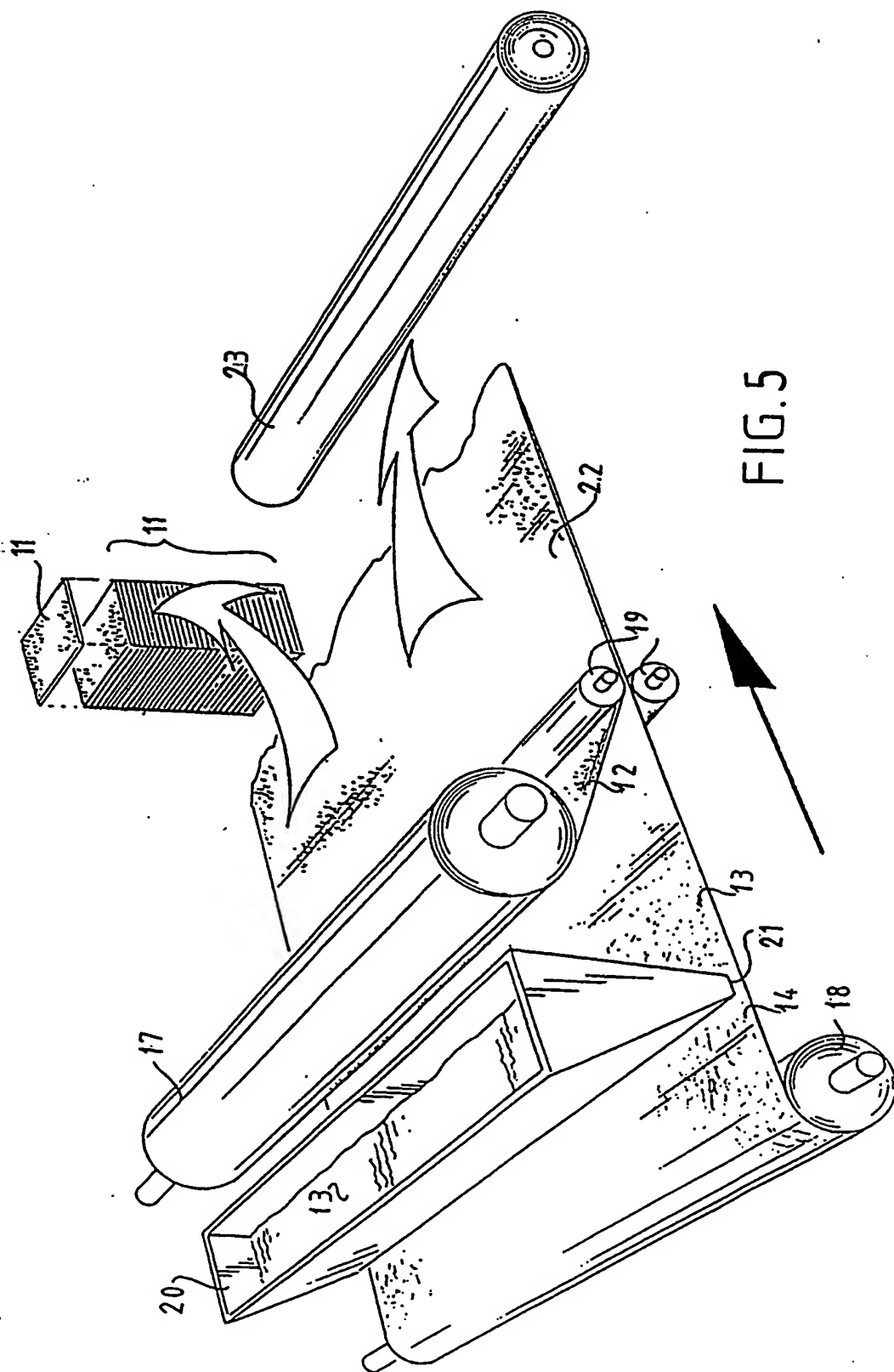


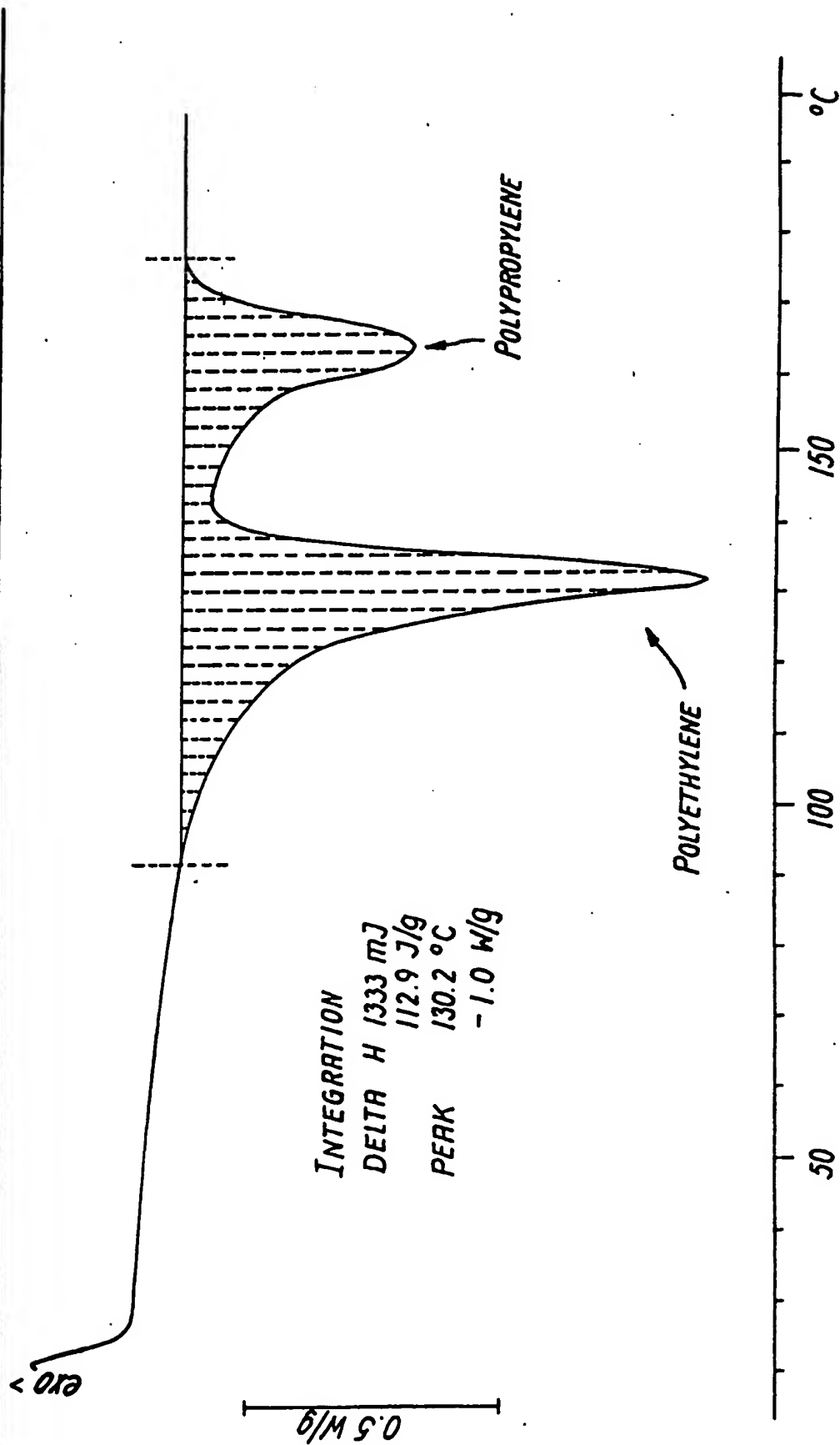
FIG. 5

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FIG.6 Bi-component (polypropylene/polyethylene fibre

11.800 mg

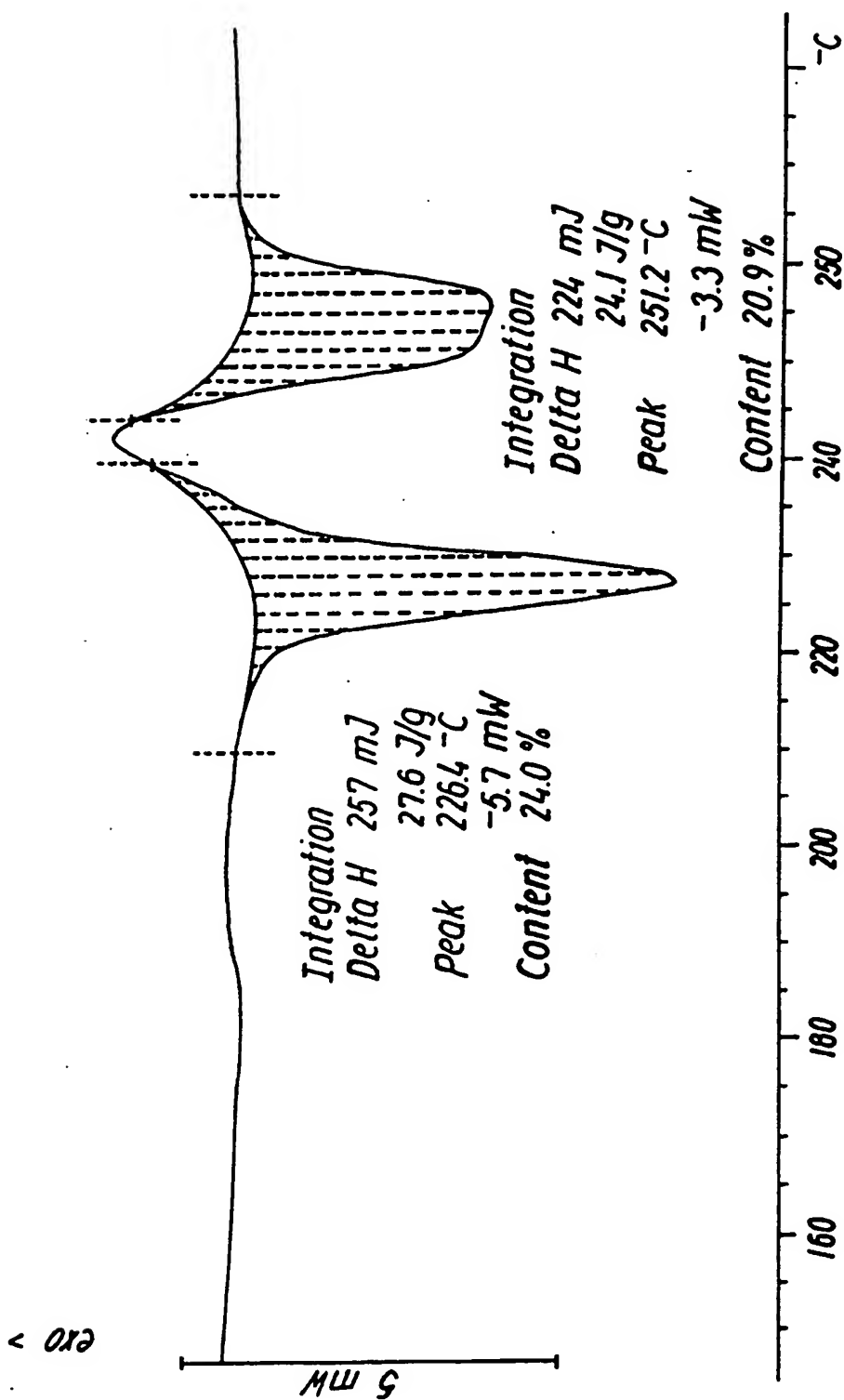
RATE: 10.0 °C/min



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FIG.7 Bi-component Polyester fibre

9.300 mg Rate: 100 °C/min



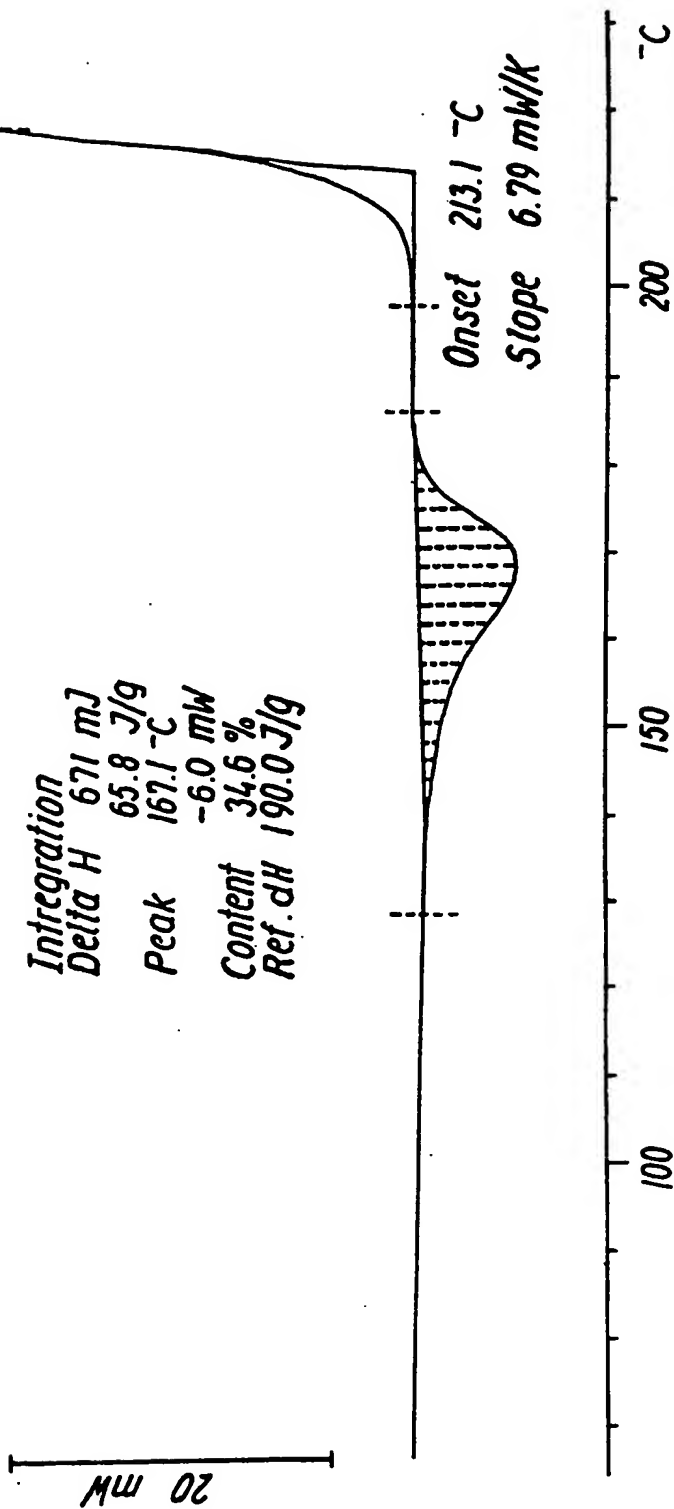
7/11

FIG. 8 Polypropylene fibre

Oxygen
Rate: 10.0 °C/min

10.200 mg

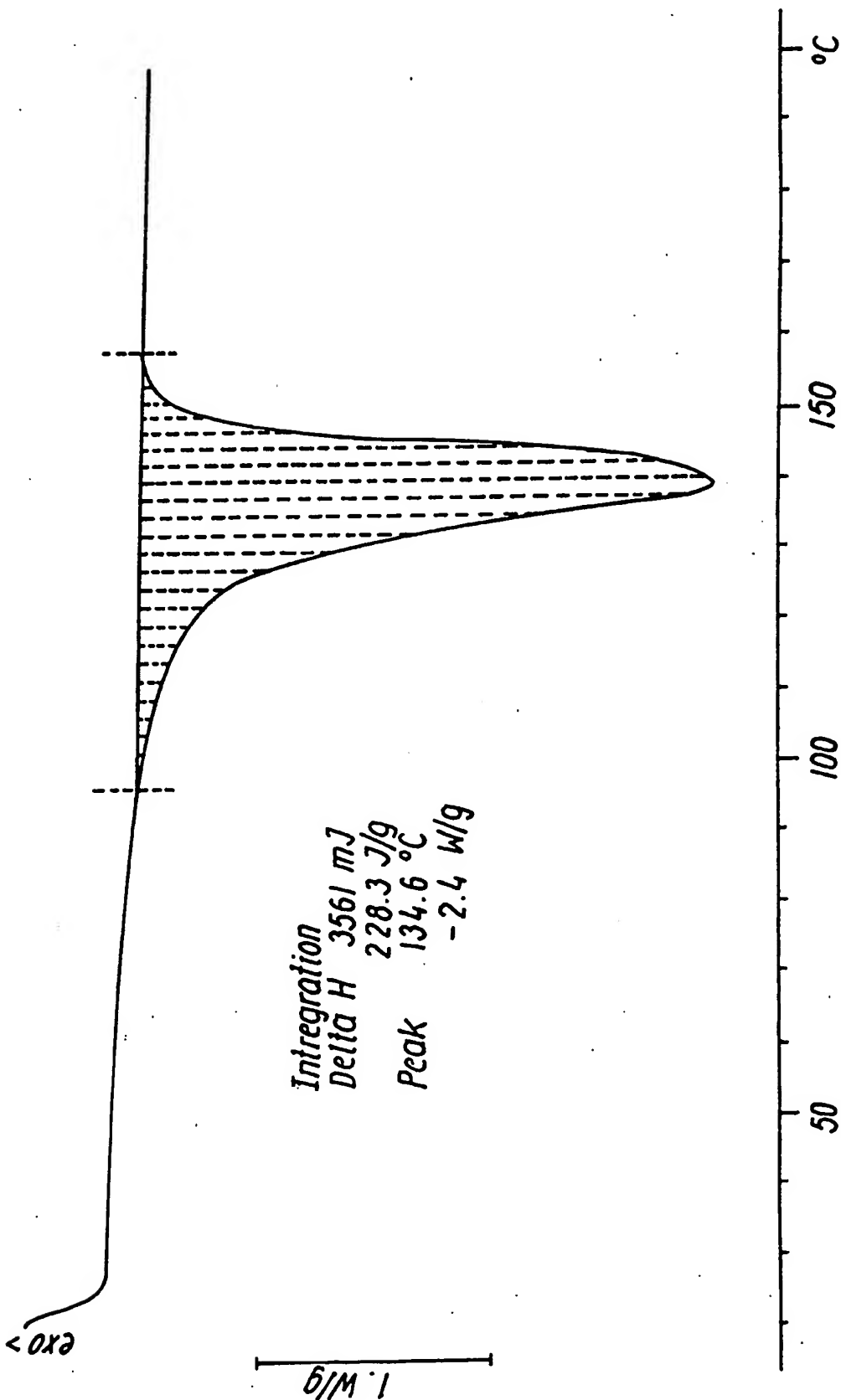
exo >



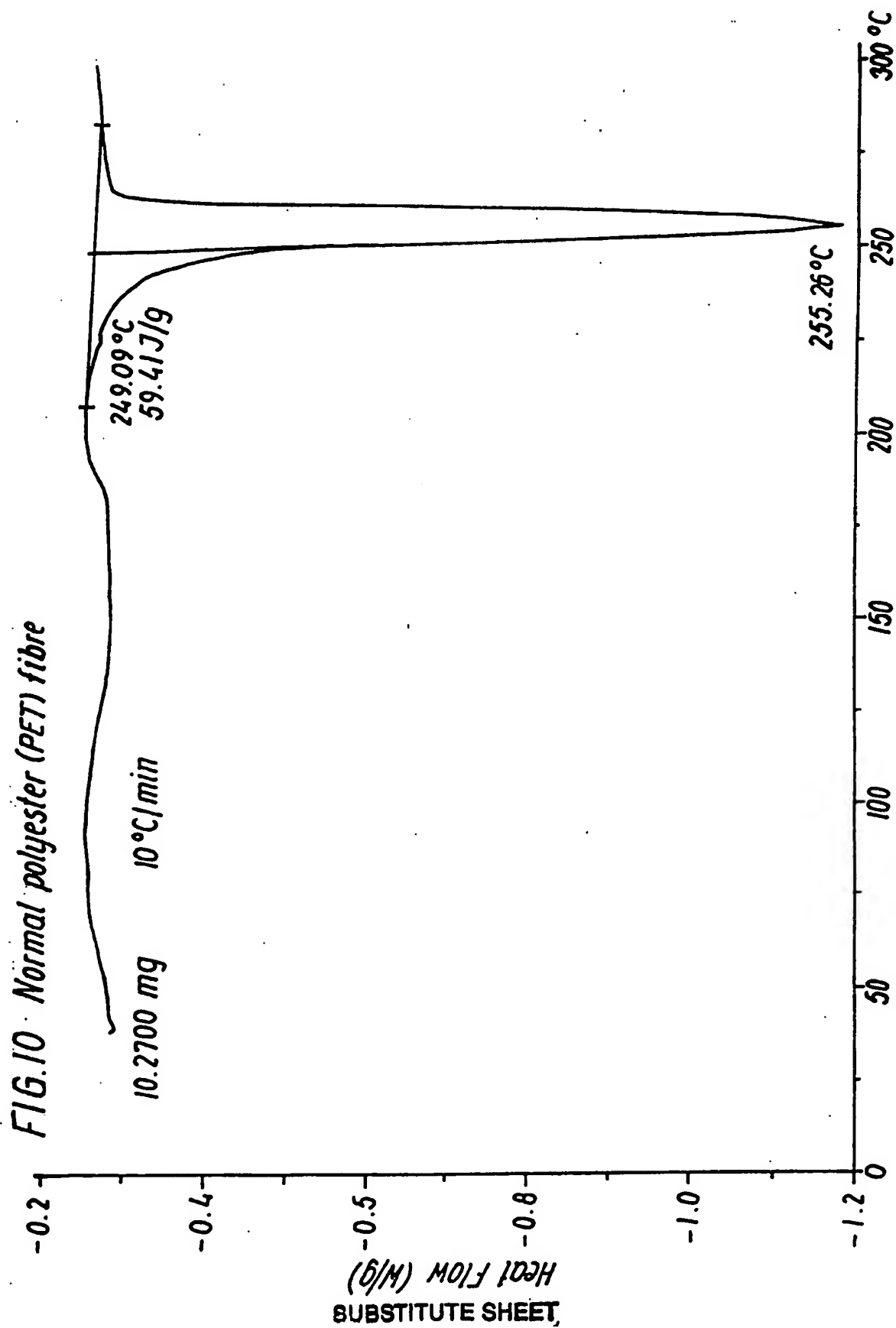
8/11

FIG.9 HD-Polyethylene fibre

15.600 mg Rate: 10.0 °C/min



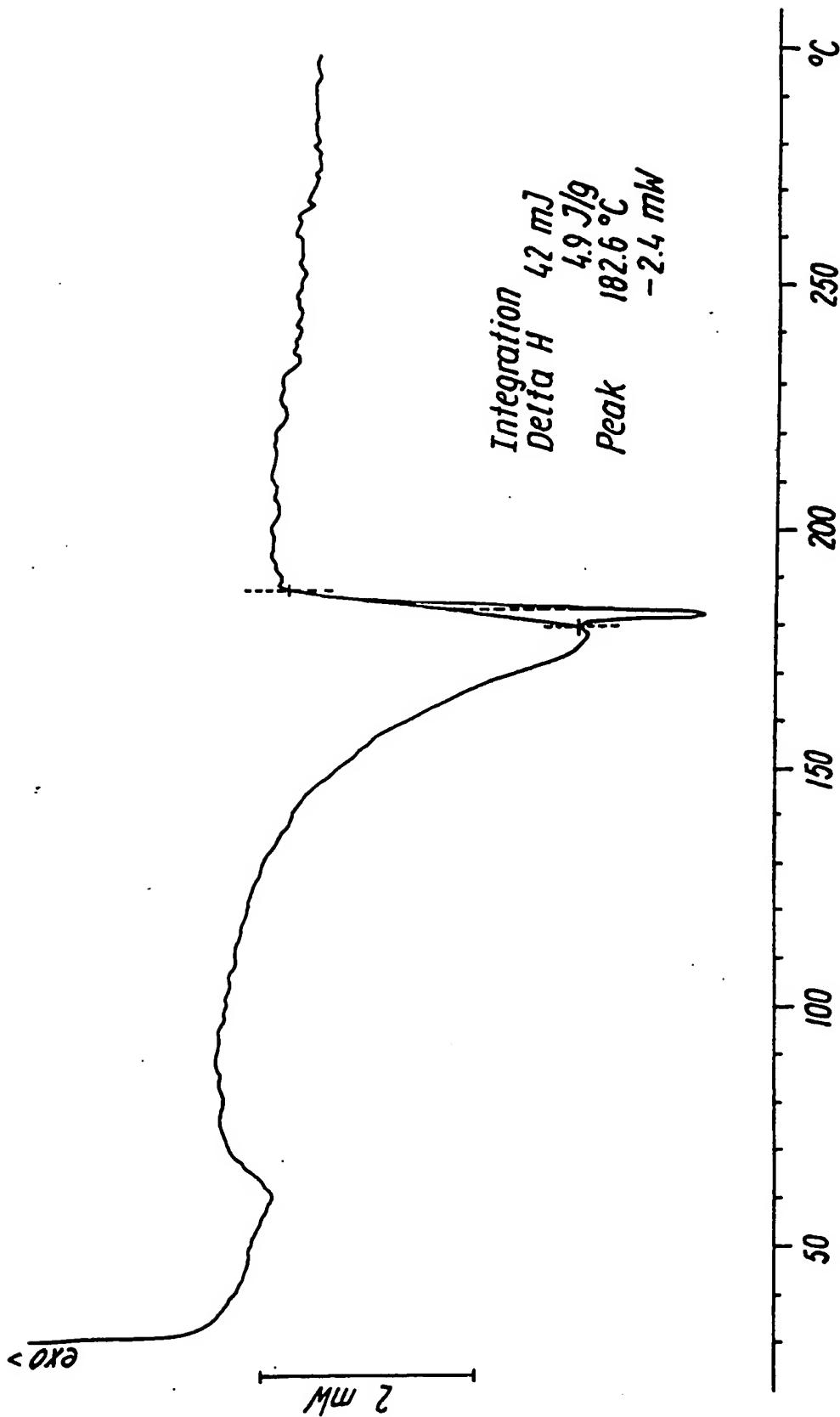
9/11



10/11

FIG. 11 Co - polyester fibre

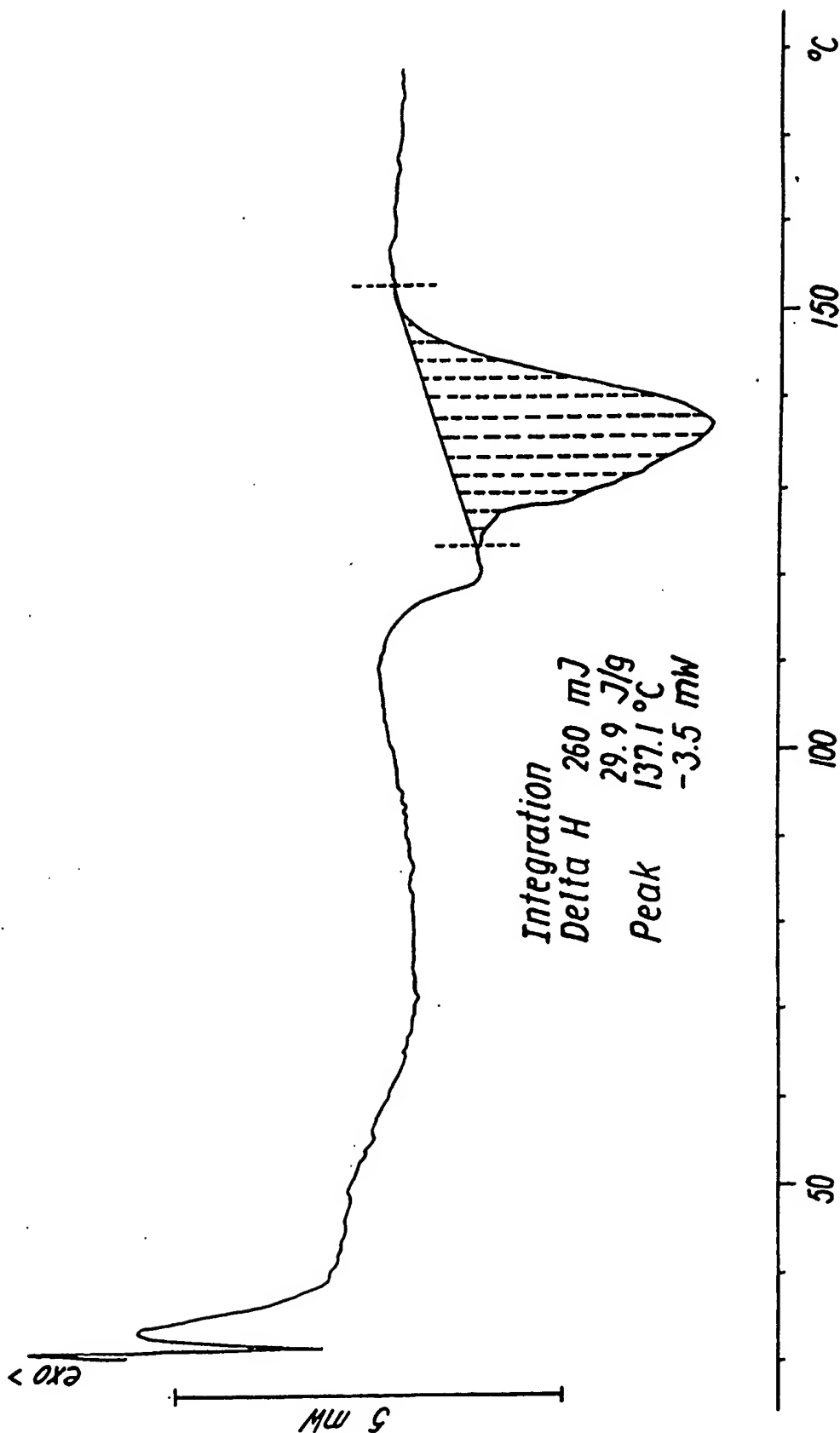
8.600 mg Rate: 10.0 °C/min



11/11

FIG. 12 Co-polyamide fibre

8.700 mg Rate: 10.0 °C/min



INTERNATIONAL SEARCH REPORT

International application No.

PCT/DK 94/00326

A. CLASSIFICATION OF SUBJECT MATTER		
IPC6: D06N 7/00, A47G 27/00, B32B 27/04 According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED		
Minimum documentation searched (classification system followed by classification symbols)		
IPC6: D06N		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
SE,DK,FI,NO classes as above		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP, A1, 0547533 (AMOCO FABRICS ZWEIGNIEDERLASSUNG DER AMOCO DEUTSCHLAND GMBH), 23 June 1993 (23.06.93), column 2, line 4 - line 13; column 3, line 12 - line 15; column 3, line 49 - line 53, claim 11	1-19,26-27
Y	--	20-25
Y	US, A, 4342813 (WAYNE K. ERICKSON), 3 August 1982 (03.08.82), column 1, line 24 - line 25; column 1, line 63 - line 66; column 6, line 39 - line 42	20-25
A	--	1-19
<input checked="" type="checkbox"/> Further documents are listed in the continuation of Box C. <input checked="" type="checkbox"/> See patent family annex.		
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C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP, A2, 0005050 (TAY TEXTILIES LIMITED), 31 October 1979 (31.10.79), page 4, line 8 - page 5, line 19, abstract --	1-27
A	EP, A2, 0278690 (HEUGA HOLDING BV), 17 August 1988 (17.08.88), abstract --	1-27
A	EP, A2, 0420661 (HEUGA HOLDING BV), 3 April 1991 (03.04.91), abstract -- -----	1-27

INTERNATIONAL SEARCH REPORT

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Patent document cited in search report		Publication date	Patent family member(s)		Publication date
EP-A1-	0547533	23/06/93	DE-U-	9115657	20/02/92
US-A-	4342813	03/08/82	NONE		
EP-A2-	0005050	31/10/79	NONE		
EP-A2-	0278690	17/08/88	AU-B-	590469	02/11/89
			AU-A-	1131188	11/08/88
			JP-A-	63264983	01/11/88
			US-A-	4702950	27/10/87
EP-A2-	0420661	03/04/91	AU-B-	632368	24/12/92
			AU-A-	6314590	11/04/91
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